

Origins and consequences of asymmetric nano-FTIR interferograms

GERGELY NÉMETH,^{1,2,*} HANS A. BECHTEL,^{3,\$} AND FERENC BORONDICS,^{1,#}

¹SOLEIL Synchrotron, L'Orme des Merisiers, RD128, Saint Aubin, France 91190

²Wigner Research Centre for Physics, 29-33 Konkoly-Thege str. Budapest, Hungary, 1121

³Advanced Light Source, Lawrence Berkeley National Laboratory, 1 Cyclotron Road, Berkeley, CA USA 94720

*gergely.nemeth@synchrotron-soleil.fr, \$habechtel@lbl.gov, #ferenc.borondics@synchrotron-soleil.fr

Abstract:

Infrared scattering-type near-field optical microscopy, IR s-SNOM, and its broadband variant, nano-FTIR, are pioneering, flagship techniques for their ability to provide molecular identification and material optical property information at a spatial resolution well below the far-field diffraction limit, typically less than 25 nm. While s-SNOM and nano-FTIR instrumentation and data analysis have been discussed previously, there is a lack of information regarding experimental parameters for the practitioner, especially in the context of previously developed frameworks. Like conventional FTIR spectroscopy, the critical component of a nano-FTIR instrument is an interferometer. However, unlike FTIR spectroscopy, the resulting interference patterns or interferograms are typically asymmetric. Here, we unambiguously describe the origins of asymmetric interferograms recorded with nano-FTIR instruments, give a detailed analysis of potential artifacts, and recommend optimal instrument settings as well as data analysis parameters.

1. Introduction

Infrared spectroscopy has been dominated by Fourier-transform (FT) instruments shortly after the first commercial FTIR spectrometer appeared on the market in the 1960s. [1] Seminal works of Fellgett [2] and Jacquinot [3] established the advantages of spectroscopic interferometry over grating instruments and led to a general layout where the radiation probing the sample is conditioned by first passing through an interferometer; in modern instruments, most frequently using a configuration introduced by Michelson and Morely, *a.k.a. the Michelson interferometer*. [4] Today, such Fourier-transform infrared instruments are ubiquitous in both industrial and scientific settings and contribute to a plethora of research. They provide easy access to rotational, vibrational and electronic absorption spectra. However, to determine complex value functions, e.g., the complex refractive index (\tilde{n}), one needs to apply the Kramers-Kronig transformation, [5,6] which require low- and high-energy extrapolations as the integrals are formulated from zero to infinity.

In the 1960s, an alternative method, called Dispersive Fourier Transform Spectroscopy (DFTS), was developed to more directly determine complex optical functions, achieved by placing the sample inside the interferometer (Fig. 1). [7,8] This asymmetric Michelson interferometric approach was further developed through the late 1980s [9–11], but it was never commercialized due to technical limitations at the time, [12] as well as a relatively limited commercial gain over existing solutions.

Both FTIR and DFTS instruments measure a real-value dataset: the detector intensity as a function of the optical path difference (OPD) of the two interferometer mirrors. The resulting interferogram is subsequently Fourier-transformed to yield a complex-value dataset. In FTIR the phase is not related to the sample and reflects the interferometer's characteristics (inaccuracies of optical elements, misalignment, beamsplitter dispersion) and sampling inaccuracies. Most often, the phase interferogram is used to maximize the amplitude algorithmically. [1] In contrast, the

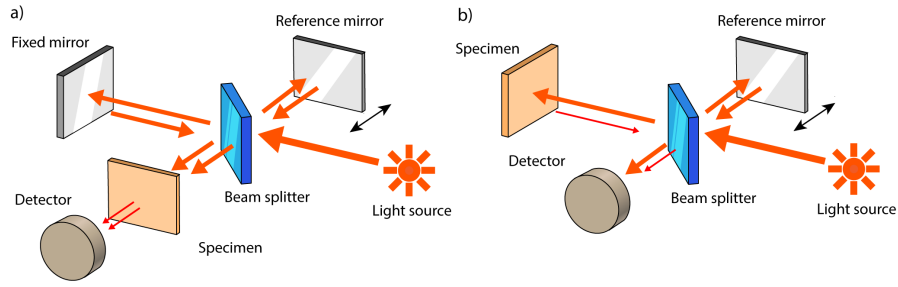


Fig. 1. Schematics of the arrangement (a) conventional FTIR and (b) DFTS setups. In the case of simple FTIR the sample is located after the interferometer, while in the case of DFTS the sample is inserted in the arm with the fixed mirror. Reflective samples can replace the fixed mirror completely (like in b), while in transmission mode the sample is inserted between the fixed mirror and the beamsplitter.

phase spectrum in DFTS, where the light passes through the sample inside the interferometer and thus suffers a particular phase shift, carries information about the sample. By using the amplitude and phase information, DFTS instruments can directly measure the complex dielectric response of a material.

Although DFTS was never commercialized, another IR microscopy technique, scattering-type Scanning Near-field Optical Microscopy (s-SNOM), uses the same asymmetric Michelson arrangement and has achieved commercial success. This technique enables infrared spectroscopic measurements at the nanoscale, with a spatial resolution of several orders of magnitude better than diffraction-limited, far-field infrared techniques.

1.1. Scattering SNOM and nano-FTIR

A typical s-SNOM setup consists of an infrared source and an atomic force microscope (AFM) located within an asymmetric Michelson interferometer. In this case, the fixed mirror is replaced by the ensemble of a focusing mirror, the AFM tip, and the sample, as depicted in Fig. 2. Light enters the interferometer and the beamsplitter directs half the light to the moving reference mirror while the other half is focused onto the apex of the AFM tip. When the sample is brought into close proximity of the tip, the optical fields locally interact in the near field and cause scattering that can be detected in the far field. The scattered light is collected by the same focusing mirror and recombined with the light from the reference mirror before being measured by an infrared detector. The interaction volume is defined by the AFM tip sharpness, and is usually on the order of tens of nanometers, allowing spatial resolution well beyond the far-field diffraction limit.

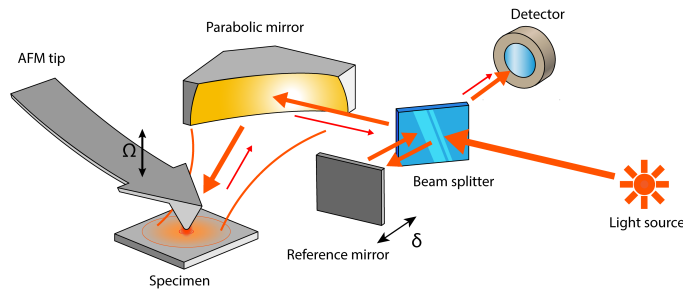


Fig. 2. Schematic representation of a s-SNOM setup.

67 To separate the weak near-field scattering from the intense background scattering, s-SNOM
68 measurements combine higher harmonic demodulation and interferometric signal amplification.
69 The AFM operates in tapping mode to modulate the scattering amplitude and the detector
70 signal is demodulated at harmonics of the tip oscillation frequency ($n\Omega$). Because the near-field
71 interaction is non-linear with sample distance, higher harmonic detection leads to suppression of
72 the far-field scattered light, which is nominally linear with sample distance. Additionally, mixing
73 the back-scattered light (E_N) with the beam from the reference mirror of the interferometer (E_R)
74 results in signal level enhancement by $E_N E_R$ and phase modulation in the interference term.
75 With monochromatic illumination, the reference mirror movement is typically modulated at a
76 fixed frequency in a pseudo-heterodyne detection scheme that further suppresses background and
77 extracts the amplitude and phase of the near-field scattering [13]. For broad-band illumination,
78 the reference mirror is moved linearly over a fixed distance and the demodulated signal is
79 recorded as a function of mirror position to collect an interferogram. The subsequent nano-FTIR
80 interferogram is then Fourier-transformed to yield the amplitude and the phase of the scattered
81 light. [14]

82 Here, we will discuss the analogies between DFTS and s-SNOM and unambiguously explain
83 the origin and practical consequences of the recorded asymmetric interferogram.

84 2. Origin of the asymmetry

85 In a Michelson interferometer, the beamsplitter divides the incoming beam in two (we consider
86 an ideal 50:50 beamsplitter). Considering broadband illumination, the incoming collimated
87 beam contains a broad range of wavelength components. The interferogram is the sum of the
88 interference patterns of the individual wavelength components. First, let us consider a single
89 wavelength component. Its electric field is described as

$$\mathbf{E}(\mathbf{r}, t) = \mathbf{E}_0 \exp [i(\Phi_r(k) + \mathbf{k} \cdot \mathbf{r} - \omega t)] . \quad (1)$$

90 The part of the beam that is directed to the reference arm of the interferometer is reflected back
91 by a moving mirror and written as

$$\mathbf{E}_R(\mathbf{r}, t) = \frac{1}{2} \mathbf{E}_0 \exp [i(\Phi_r(k) + \mathbf{k} \cdot \mathbf{r} - \omega t + k \cdot \delta)] , \quad (2)$$

92 where $\delta/2$ is the displacement of the moving mirror from the zero path difference position of the
93 two arms and $\Phi_r(k)$ is a random initial phase for each wavelength component.

94 In the asymmetric setup, the sample is located in the stationary interferometer arm. The
95 interaction of the light with the sample is described by the complex insertion loss in DFTS
96 and formulated as $L(k) \exp [\Phi_L(k)]$. The exact expression of the insertion loss depends on the
97 interaction that influences the backward propagation of the electromagnetic field in this arm. For
98 s-SNOM, the dominant effect is the back-scattering, originating from the tip-sample interaction.
99 The scattered field from the sample arm is

$$\mathbf{E}_S(\mathbf{r}, t) = \frac{1}{2} \mathbf{E}_0 L(k) \exp [i(\Phi_r(k) + \mathbf{k} \cdot \mathbf{r} - \omega t + \Phi_L(k))] . \quad (3)$$

100 Note, that the initial $\Phi_r(k)$ random phase remains the same in both arms because the Michelson
101 interferometer with an ideal beamsplitter realizes only amplitude division. Finally, the split
102 beams recombine, and the electric field at the detector can be written as

$$\mathbf{E}_D(r, t) = g(k, x) \exp [i(\mathbf{k} \cdot \mathbf{r} - \omega t)] , \quad (4)$$

103 where

$$\mathbf{g}(k, x) = \frac{1}{2} \mathbf{E}_0(k) (L(k) \exp [i\Phi_L(k)] + \exp [ik\delta]) . \quad (5)$$

104 The detector intensity is proportional to $\mathbf{E}_D \mathbf{E}_D^*$, which leads to

$$I_D(k, \delta) = \frac{1}{4} [1 + L^2(k)] \mathbf{E}_0(k) \mathbf{E}_0^*(k) + \frac{1}{2} L(k) \cos [\Phi_L(k) - k\delta] \mathbf{E}_0(k) \mathbf{E}_0^*(k). \quad (6)$$

105 Here, the second term describes the interference and it is recorded as the mirror is moving
 106 (changing δ). The amplitude of the recorded cosine interferogram is set by the amplitude $L(k)$
 107 of the loss function, while its phase is controlled by the phase shift $\Phi_L(k)$.

108 For incoherent, broadband illumination, the full interferogram is the incoherent sum of all the
 109 individual cosine interferograms of each wavelength component.

$$I_D(\delta) = \int_{-\infty}^{\infty} I_D(k, \delta) dk = \quad (7)$$

$$\int_{-\infty}^{\infty} \frac{1}{4} [1 + L^2(k)] I_0(k) dk + \int_{-\infty}^{\infty} \frac{1}{2} L(k) I_0(k) \cos [\Phi_L(k) - k\delta] dk, \quad (8)$$

110 where $I_0(k) = \mathbf{E}_0(k) \mathbf{E}_0^*(k)$ is the intensity of the incoming radiation. The first term of Eq. 8
 111 is independent of the reference mirror position δ and thus gives only a constant offset to the
 112 interferogram. The varying part of the interferogram which contains information is the second
 113 term. From Eq. 8, we see that $L(k)$ changes the amplitude while $\Phi_L(k)$ shifts each component
 114 compared to the ZPD position. This results in a significant change in the shape of the full
 115 interferogram. In the end, we see that the complex insertion loss $\hat{L}(k) = L(k) \cdot \exp i\Phi_L(k)$ drives
 116 the asymmetry. The exact formula for the insertion loss is defined by the physical interaction
 117 between the sample and the incoming light. We showcase the effect of insertion loss on the
 118 interferogram in Fig. 3.

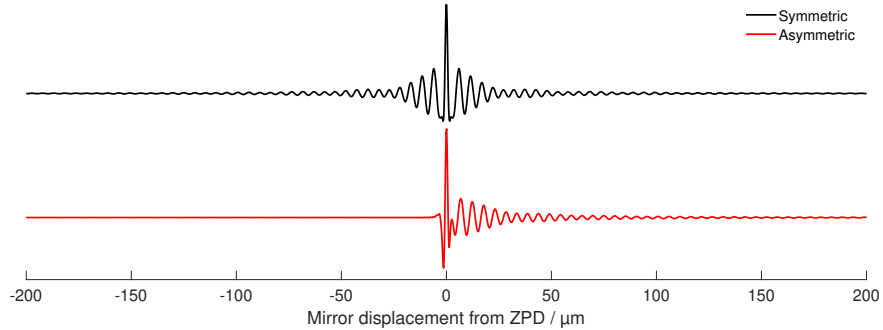


Fig. 3. Comparison of symmetric (conventional FTIR) and asymmetric (DFTS) interferograms. It considers a reflective half-infinite SiC mirror placed after the interferometer (symmetric) or in the interferometer, replacing the fixed mirror (asymmetric)

119 In the following, we consider a DFTS arrangement with a SiC sample in the position of
 120 the fixed mirror. The loss function in this case is defined as the Fresnel reflection coefficient.
 121 For the sake of simplicity, we assume normal incidence, thus the insertion loss becomes
 122 $\hat{L}(k) = r(k) = (n_{SiC}(k) - 1)/(n_{SiC}(k) + 1)$. Using (8) and ignoring the DC part of the signal,
 123 we get the highly asymmetric interferogram shown as the red curve of Fig. 3.

124 From Fig. 3, we see that the asymmetry modifies the positive pathlength difference part of
 125 the interferogram. The reason for this is that physical processes like scattering, reflection, and
 126 emission always induce a positive phase shift due to causality.

127 In DFTS interferograms the asymmetry contains information about the sample's complex
 128 optical properties, while in conventional FTIR, the phase spectrum (phase of the Fourier transform
 129 of the interferogram) does not tell anything about the sample.

The insertion loss of a sample can be retrieved through a reference measurement as follows:

$$\hat{L}(k) = \int_{-\infty}^{\infty} I_S(\delta) \exp(2\pi i k \delta) d\delta / \int_{-\infty}^{\infty} I_R(\delta) \exp(2\pi i k \delta) d\delta \quad (9)$$

$$= FT(I_S(\delta)) / FT(I_R(\delta)), \quad (10)$$

130 where the subscripts S and R stand for sample and reference, respectively.

131 Furthermore, if the complex insertion loss is linearly related to the optical functions of the
 132 sample, DFTS provides a direct measurement.

133 2.1. Nano-FTIR interferograms

134 We can explain the nano-FTIR interferogram in the framework of DFTS presented above. The
 135 key is to find the insertion loss that describes the scattering of the tip-sample ensemble. The
 136 calculation of the amplitude and phase of the back-scattered light can be done in different ways
 137 as numerous theoretical methods have been used to approximate the solution of the scattering
 138 problem. [15–23] A widely used and easily implementable tip-sample interaction model, the
 139 so-called finite dipole model (FDM) treats the problem with a quasi-electrostatic approach and
 140 describes the main characteristics of the scattering almost quantitatively. [21]

141 The main quantity that we are looking for is the complex scattering coefficient $\sigma(k)$ which
 142 relates the incoming and the back-scattered fields by $E_s = \sigma(k)E_{inc}$. The FDM model provides
 143 a closed-form solution for the scattering coefficient. [21] σ inherits its wavelength dependence
 144 from the dielectric function of the sample. As σ characterizes the backward propagating optical
 145 field, it can be used as the insertion loss we were looking for.

146 In a real measurement, however, the acquired signal is not directly proportional to the scattering
 147 coefficient. The detected signal contains a significant background component hindering the
 148 tip-scattered light originating from the near-field interaction. To retrieve the pure near-field
 149 signal, the AFM works in tapping mode vibrating the tip at frequency Ω . Then, the acquired
 150 time-dependent signal is then demodulated at higher harmonics $n\Omega$. To gather a similar quantity
 151 from the FDM model, we implement the modulation for the scattering coefficient σ . Then,
 152 similarly to the real measurement by demodulating the time-dependent signal at the n th harmonic
 153 of Ω , we get σ_n .

154 By using the FDM model to derive $\sigma_n(k)$ and substituting it for the insertion loss we can
 155 calculate the nano-FTIR interferograms and assess their asymmetry. To showcase the effect
 156 of different material responses we created a dielectric function to model theoretical material
 157 possessing three typical excitation types in the mid-infrared spectral range. We used this to
 158 calculate the amplitude and phase of the 2nd harmonic scattering coefficient. This dielectric
 159 function and the scattering spectrum can be viewed in Fig. S1. At around zero frequency, we
 160 added a typical Drude excitation, at 800 cm^{-1} a surface polariton excitation, and at 1423 cm^{-1}
 161 we imitate a simple vibrational excitation where the real part of the dielectric function remains
 162 positive.

163 For a Lorentzian oscillator with only positive real values, the scattering phase follows the
 164 shape of the imaginary part of the dielectric function. This is usually the case of weak molecular
 165 vibrations. The phase of the scattering signal is sensitive and grows large when the real part of
 166 the dielectric function falls below zero, which is typical for collective excitations like surface
 167 polaritons. This sensitivity makes s-SNOM ideal to study surface excitations, which is shown
 168 by the numerous publications from studies on plasmons in graphene and carbon nanotubes to
 169 phonons in polar dielectrics [24–31].

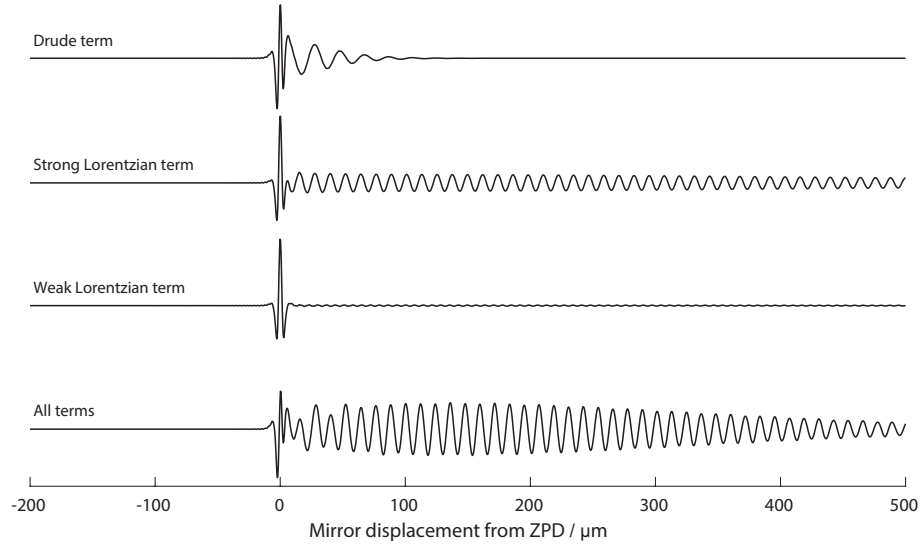


Fig. 4. Model interferograms based on Eq. 8, composed of different terms from the model dielectric function to determine the scattering coefficient using FDM model.

Based on Eq. 8, the stronger and broader the scattering phase spectrum, the more asymmetry will appear in the interferogram. To provide insight into this statement, in Fig. 4 we present the calculated interferograms for theoretical materials exhibiting only one of the above-mentioned excitations at a time. Fig. 4 shows how the broad Drude peak introduces pronounced asymmetry with a fast decay of the interferogram while the similarly strong, but narrower Lorentzian peak introduces a much longer-lasting interferogram for the positive path lengths. With the weak oscillator, the asymmetry is not that clear as the phase shift is small and concentrated only to a few wavelengths.

3. Model validation

To validate our description of the interferograms, we modeled and measured the nano-FTIR interferogram of 300 nm SiO₂ layer on top of silicon. The broadband s-SNOM measurements were done at the SMIS beamline of the SOLEIL synchrotron, the French national synchrotron facility, with a commercial s-SNOM manufactured by Attocube system AG (Haar, Germany). The incident synchrotron radiation was split by a ZnSe beamsplitter and the transmitted beam was focused on the apex of a platinum-coated AFM tip by an off-axis parabolic mirror. The reflected part of the beam entered the reference arm with the moving mirror actuated by a piezo stage capable of moving 800 μm . We recorded the full interferogram of the thermally grown SiO₂ layer using the full range of the piezo actuator acquiring 2048 points which resulted in 0.39 μm spatial sampling. The integration time for each pixel was 13 ms and the tapping amplitude of the tip was set to 100 nm. Data was recorded for higher-harmonics up to the 4th order but in the following, we use 2nd harmonic near-field signals in our analysis.

For modeling, we used FDM as described above to calculate the second harmonic demodulated amplitude and phase spectrum to derive the interferograms. The dielectric function for the SiO₂ layer was obtained from the literature model reported by Kischkat et al. [32]. Fig. S2 renders the dielectric function and the second harmonic amplitude and phase spectra that was used in the interferogram calculation. The DFTS insertion loss is defined as $L_n(k) = \sigma_n(k) = s_n(k) \exp[i\varphi_n(k)]$, where $s_n(k) = s_{n,\text{SiO}_2}/s_{n,\text{Au}}$ and $\varphi_n(k) = \varphi_{n,\text{SiO}_2} - \varphi_{n,\text{Au}}$, because all the data in the measurements were normalized to a reference measurement on gold. In all of our

198 studies, both calculated and measured amplitude and phase values were normalized to that of
 199 gold substrates. We expect a definite asymmetry with moderate decay caused by the broad,
 200 intense phase peak ranging from around 1100 cm^{-1} to 1500 cm^{-1} originating from the phonon
 201 band of the SiO_2 .

202 Our calculations describe the corresponding measurements nearly perfectly. Fig. 5 shows the
 203 comparison of the model result (black) and the measured interferogram (red). The interferogram
 204 was calculated by Eq. 8 using the second harmonic scattering coefficient as the insertion loss
 205 described above. The small difference between the two curves can originate from the inaccuracy
 206 of the dielectric function of the SiO_2 layer and the limitations of the simple FDM model. Still,
 207 with these limitations, the DFTS-based interferogram calculation described above can reproduce
 208 and explain the asymmetry of nano-FTIR interferograms extremely well.

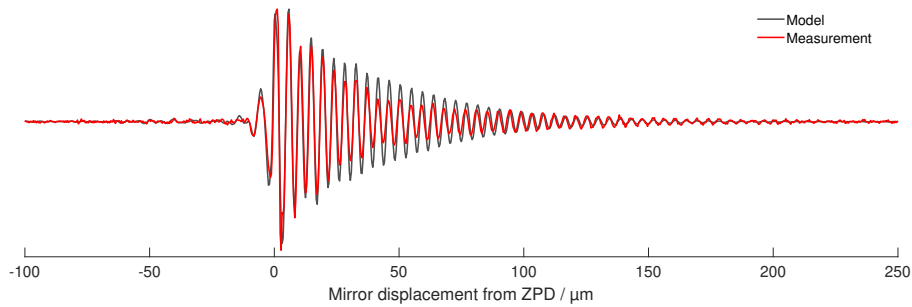


Fig. 5. Measured (red) and calculated (black) interferogram of the 300 nm SiO_2/Si sample.

209 As we showed in this section, our model can replicate and explain nano-FTIR interferograms,
 210 thus it can be confidently used to explore the effect of various measurement artifacts and
 211 data-processing schemes on the final spectrum. In the following, we discuss the most important
 212 considerations one has to make during measurements and the processing of raw interferograms.

213 3.1. Effect of temporal coherence

214 In real nano-FTIR setups, the light source is usually a pulsed mid-IR laser. Commercially available
 215 instruments use lasers with a pulse width $\approx 100\text{--}200\text{ fs}$, and high, MHz, repetition rate. [33–35]
 216 The advantages of these sources are the large spectral irradiance and the spatially coherent
 217 beam which makes them ideal for focusing. However, the possibility of near-field nano-FTIR
 218 measurements using thermal (Globar) sources was also demonstrated. Their advantage is the
 219 broad spectral range, but, due to their low spectral radiance and spatial coherence, the resulting
 220 near-field signal is far lower quality. [14] Alternatively, nano-FTIR spectroscopy with high-
 221 temperature plasma light sources was also demonstrated which improves the spatial coherence of
 222 thermal sources, thus providing better focusing. [36] Furthermore, a third possibility is using
 223 synchrotron sources [37] as the spectral range of a common infrared beamline ranges from the
 224 THz up to the near-IR/visible range providing high spectral radiance and diffraction-limited
 225 focusing.

226 The important difference between light sources is temporal coherence. For temporally coherent
 227 sources, such as pulsed lasers, the asymmetry of the interferogram was explained by optical free
 228 induction decay (optical FID) previously. [38] Optical FID requires the fast switch-off of the
 229 excitation or the fast detuning of the resonance of the sample thus usually measured in the time
 230 domain. [39, 40] The time delays during the re-emission process for each wavelength result in
 231 phase-shifted but coherent fields and distort the time domain shape of the back-scattered pulse,

232 which represents the impulse response function of the sample. In the asymmetric Michelson-
233 interferometer arrangement, the cross-correlation of the original and the back-scattered pulses is
234 recorded as the interferogram.

235 However, thermal sources or typical synchrotron radiation don't provide temporally coherent
236 pulses, i.e., the phase between the different wavelength components varies randomly ($\Phi_r(k)$
237 in Eq. 2 and 3).¹ The final interferogram, however, looks the same as with coherent excitation.
238 This is because a Michelson interferometer realizes amplitude division thus the initial phase
239 $\Phi_r(k)$ is the same in both arms and does not play a role in the interferogram formation. This
240 means that formally both coherent and incoherent cases result in the same formula (Eq. 8) and
241 the interferograms look the same.

242 We want to note that in both cases the origin of the asymmetric interferogram is the phase
243 shift of each wavelength component by the scattering process. FID signal is a special case when
244 using coherent radiation, but the resulting interferogram is the same with or without temporal
245 coherence. In Fig. S4, we show this in detail for coherent and incoherent sources.

246 4. Implications for measurement and data processing

247 In FTIR, as shown by Eq. 10, the frequency response of the sample is calculated by Fourier
248 transforming the interferogram. As extensively, and widely described, the preprocessing of the
249 interferograms before Fourier transformation is a critical step to suppress artifacts caused by the
250 effective boxcar windowing of the ideal interferogram originating from the finite path length
251 range of the moving mirror. [1]

252 Since the resulting spectrum is the convolution of the frequency spectrum of the window
253 function and the ideal spectrum, it is advantageous to apply a custom window function that has a
254 narrow frequency spectrum and small side lobes. This process is called apodization and is widely
255 used in FTIR spectroscopy. [1] One of the concerns in nano-FTIR (or DFTS) is how and what
256 type of apodization to apply before the Fourier transform. Our main goal is to preserve the shape
257 of the interferogram as much as possible because it contains the phase information of the sample.

258 4.1. Position of the ZPD and apodization

259 To collect as much useful information as possible, earlier works suggested setting the interferometer
260 scanner range such that more of the positive OPD side of the interferogram is collected. [42]
261 Thus, the ZPD position is shifted toward the beginning of the scanner range. However, it was not
262 studied, if there is an optimal ZPD shift (interferogram position). In the following, we discuss
263 this through measurements and simulations.

264 Connected to the ZPD shift, the question of the proper apodization naturally emerges. We
265 cannot use a symmetric but shifted apodization function since it would become a combination of
266 a boxcar function and the apodization function when the interferogram is shifted from the center.
267 The application of an asymmetric apodization function was suggested previously by Amenabar et
268 al., where the authors used an asymmetric three-term Blackman-Harris window. [42] This type
269 of apodization, however, changes the symmetry of the interferogram when applied incorrectly
270 and its effects were not discussed in detail before.

271 The effect of symmetry change can be dramatic on the phase spectrum. Let us suppose that the
272 interferogram is symmetric at the beginning, i.e., there is no phase shift for any of the wavelength
273 components in the broadband radiation. By shifting the ZPD position towards the beginning
274 of the scanning range (shifting to the "left") and applying asymmetric apodization, we start to
275 decrease the $\delta < 0$ side of the interferogram but keep the $\delta > 0$ side mostly untouched. In
276 the extreme case, the ZPD location is at the very beginning of the scanner range and we only

¹Storage rings can produce temporally coherent synchrotron radiation (CSR) resulting in very high-intensity THz pulses. Such sources are not considered here as CSR emission was only utilized for far-field spectroscopy measurements to date. [41]

measure the positive retardation side ($\delta > 0$) leading to a single-sided interferogram. This is equivalent to multiplying a double-sided interferogram with a Heaviside step function. The vanishing interferogram at retardations smaller than zero results in Kramers-Kronig relations in the complex spectrum. In other words, the Kramers-Kronig pair phase spectrum of the amplitude spectrum appears after the Fourier transform. [43, 44] We demonstrate this effect in supplementary Section 2. and Fig. S2 on an originally symmetric interferogram. The additional phase introduced by the symmetry change can cause severe artifacts in the final spectrum that should be avoided. In the following, we systematically study the combined effect of ZPD position change and apodization on the final spectrum.

First, we measured the nano-FTIR interferogram of SiO_2/Si samples, just like in Section 3. In NeaSCOPE instruments, the scanning mirror is attached to a manual translation stage, which we can use to shift the whole assembly with a micrometer screw. This way we can change the location of the ZPD position within the range of the piezo scanner. In all our figures zero represents the middle of the scanner range, which would correspond to the location of the ZPD in a typical FTIR measurement with symmetric IFG. A series of measurements with different ZPD positions along the scanner range are shown in Fig. 6 (a) upper panel (raw). In the post-processing, we applied an asymmetric four-term Blackman-Harris window. Fig. 6 (a) lower panel (apodized) shows the apodization functions and the apodized interferograms. We used the same apodization for the reference interferograms measured with the same ZPD positions on gold and calculated the spectra using Eq. 10. The resulting spectra are shown in Fig. 6 (b).

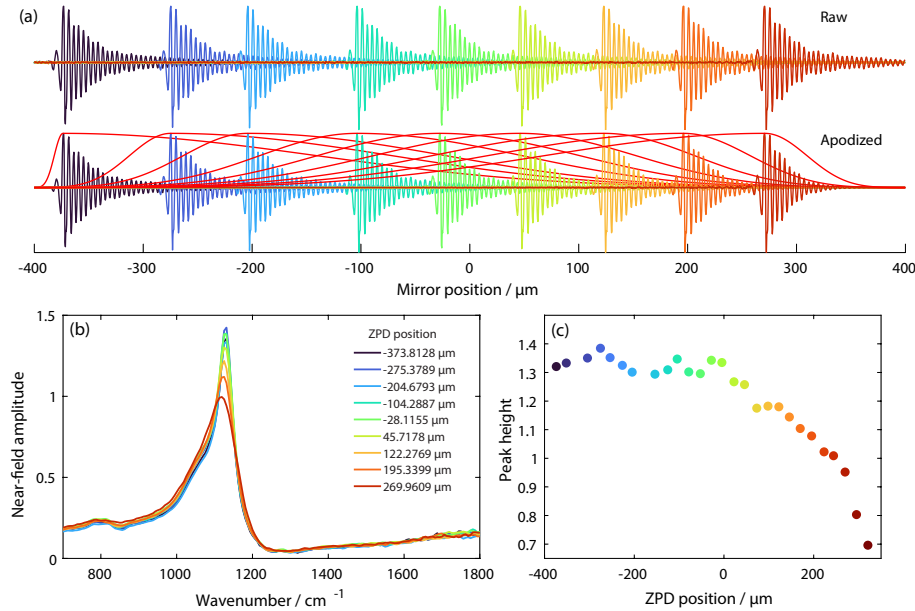


Fig. 6. (a) Measured SiO_2 near-field interferograms with different ZPD positions. (b) SiO_2 near-field spectra, calculated from the corresponding interferograms shown in (a) with different ZPD positions. (c) Magnitude of the SiO_2 phonon peak in each near-field spectra in (b).

As the interferogram is shifted to the positive side of the scanning range, the main phonon peak of silica broadens and decreases. This apparent reduction in spectral resolution is caused by the reduced interferogram length and the steeper apodization at positive values. This suggests that one should place the interferogram to the negative side of the scanning range to maximize spectral resolution for a fixed mirror scan length (and time). However, as we can see, there

is an optimum ZPD position (see in Fig. 6 (c)). If the interferogram is moved too far to the negative side, an insufficient portion of the interferogram is sampled and the rising part of the apodization function becomes so steep that even the short negative OPD side of the IFG gets distorted, resulting in a decrease in spectral peak height.

To further study the effect of the ZPD shift and the asymmetric apodization, we choose to simulate a more complex spectrum with different spectral features. We synthesized the interferograms with the help of Eq. 8 and calculated the spectra as described in Section 3. As a theoretical sample, we choose 30 nm of C_{60} fullerene molecules on top of the SiO_2/Si substrate. The spectrum then consists of the main phonon peak of the oxide and the four distinct narrow vibrational resonances of the high symmetry C_{60} molecules (526.53, 576.08, 1183.58, 1429.73 cm^{-1}). With such a complex spectrum, we can study the effects of the apodization on both the resolution and the relative spectral weights. The near-field amplitude and phase spectrum calculated by the FDM model are shown in Fig. S1. Below, Fig. 7 represents some of the interferograms and their corresponding apodization functions.

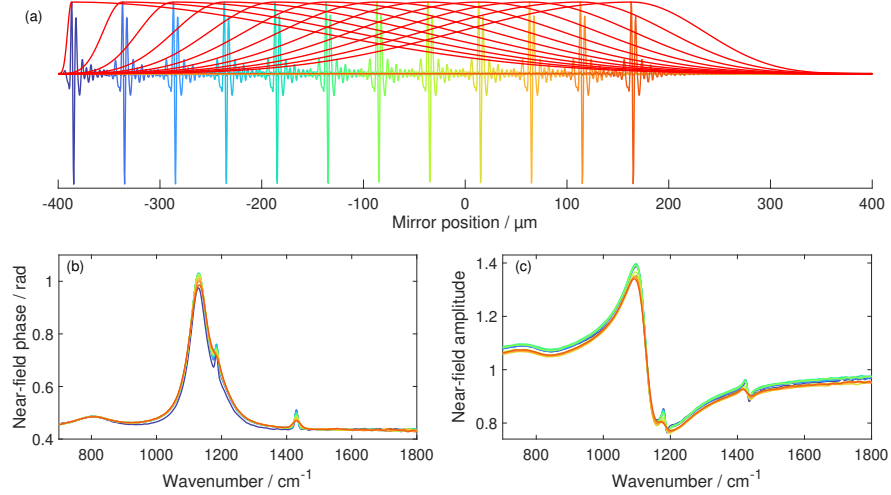


Fig. 7. (a) Calculated interferograms of the SiO_2/C_{60} layers for different ZPD positions with the corresponding asymmetric apodization function applied to them. (b) Phase and (c) amplitude spectra of the SiO_2/C_{60} system calculated from the interferograms corresponding to the color code.

In Fig. 7, we show the phase (b) and amplitude (c) spectra calculated from the interferograms displayed in (a). The main features in the spectrum are the SiO_2 phonon peak and two other peaks that correspond to the $T_{1u}(3)$ and $T_{1u}(4)$ vibrational modes of the C_{60} molecules in this spectral region. [45] The spectra clearly show that the resolution and the magnitude of the peaks decrease with increasing positive ZPD shifts, as discussed previously. For negative ZPD shifts the peak width monotonically decreases (resolution increases), however, after passing the ZPD position of $\approx -350 \mu m$ point, the 1183 cm^{-1} peak magnitude starts to decrease. Fig. 8 (a) and (b) we present the magnitude and the width of the peak at 1183 cm^{-1} , and (c) and (d) show the same values for the peak at 1429 cm^{-1} . We could see that the 1183 cm^{-1} C_{60} and the SiO_2 peak start to decrease after an optimum point but the peak 1429 cm^{-1} does not show the same behavior.

Besides our results give an insight of some trends about the effect of apodization they do not provide a clear answer if there is a specific optimum point of the ZPD position and thus the shape of the proper apodization function. Assessing only a few points of the spectrum does not describe the whole effect. The relative intensities of the peaks and the baseline of the spectra also change.

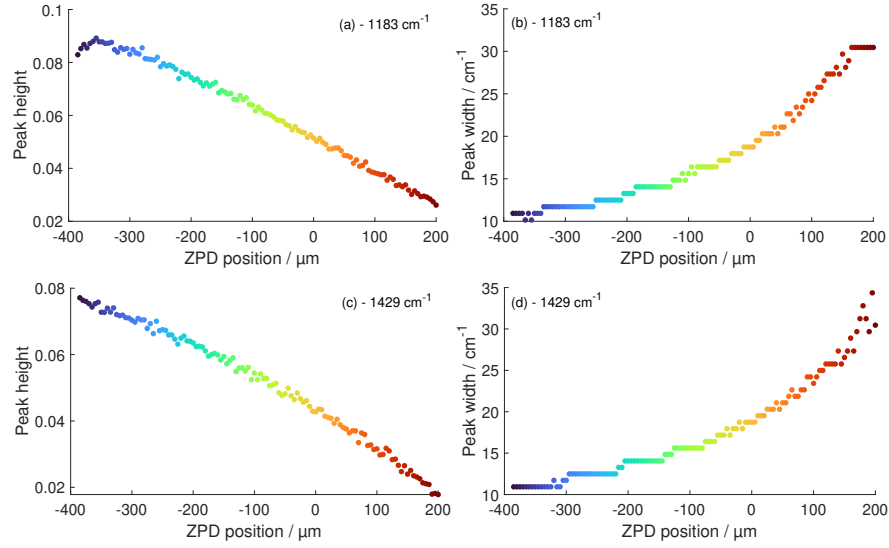


Fig. 8. (a) magnitude of the 1183 cm^{-1} C_{60} vibration, (b) width of the 1183 cm^{-1} peak, (c) magnitude of the 1429 cm^{-1} peak, (d) width of the 1429 cm^{-1} peak.

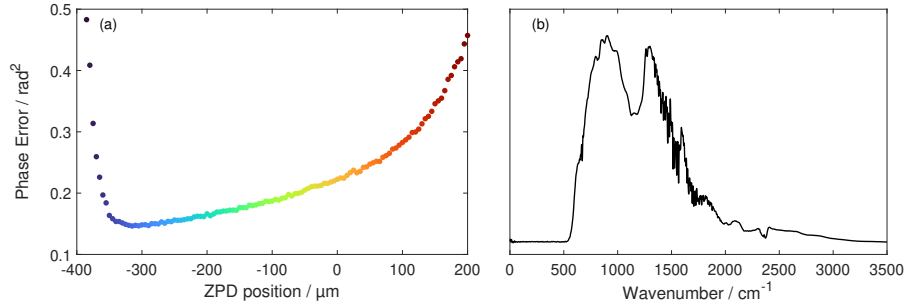


Fig. 9. (a) Error of the retrieved phase spectra compared to the ideal one for $\text{SiO}_2/\text{C}_{60}$ system, calculated from interferograms with different ZPD positions (b) Light source spectrum used in the interferogram calculations.

For this, we define a measurement of phase error where we compare the spectrum calculated from the interferograms to the ideal spectrum calculated by the FDM model. This phase error is written as $\Delta S = \int_{\nu_1}^{\nu_2} (S_{IFG}(\nu) - S_{FDM}(\nu))^2 d\nu$, where ν_1 and ν_2 are the starting and ending wavenumber of the spectral region that we are interested in. We present this measure for all the simulated interferogram-spectra calculations with different ZPD shifts in Fig. 9. The figure shows that the phase error curve has a minimum at $\text{ZPD}_{\text{shift}} \approx -335\text{ }\mu\text{m}$. The optimum ZPD shift corresponds to the minimum of the error curve. In other words, it is the optimum distance of the interferogram to the edge of the scanning range of the mirror.

The results shown above were calculated considering the broad infrared spectrum ($I_0(k)$, Fig. 9 (b)) of the SMIS beamline at Synchrotron SOLEIL, which was obtained by measuring the total signal before demodulation from a gold sample in the s-SNOM microscope. This measurement combines the effects of the source, optics, and detector to estimate the spectral response of the system. The ultrabroad wavelength range from synchrotron IR results in a

343 very narrow interferogram, as seen in the previous figures. Lab-based nano-FTIR systems,
 344 however, are typically equipped with infrared lasers based on difference frequency generation
 345 to produce an infrared output spectrum that has a much narrower spectrum than synchrotron
 346 radiation [33, 35]. This results in a much wider interferogram, which imposes an increased
 347 sensitivity to the apodization.

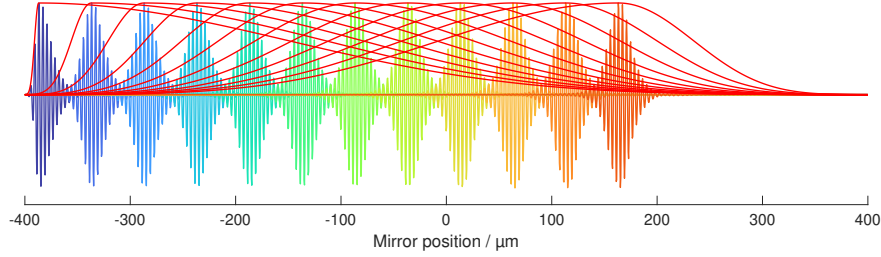


Fig. 10. Calculated interferograms of the $\text{SiO}_2/\text{C}_{60}$ layers for different ZPD positions with the corresponding asymmetric apodization function applied. The light source spectrum is shown in Fig. 11 (b) resulting in the spatially spread interferograms.

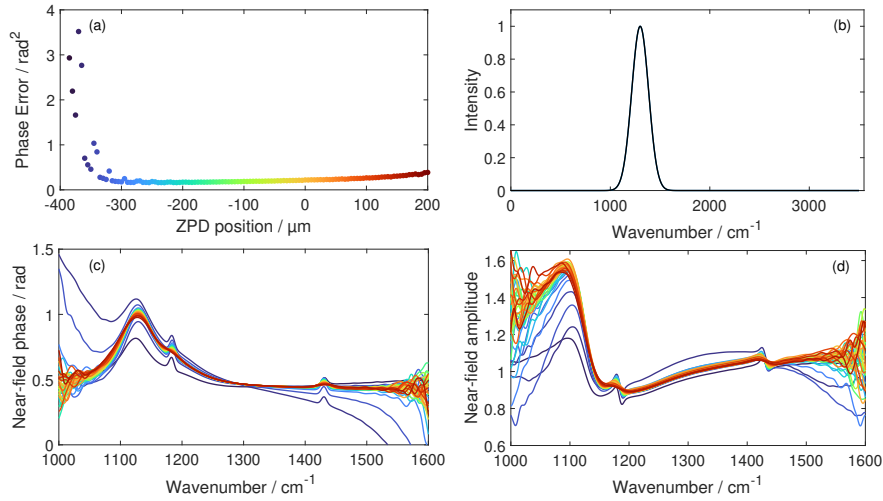


Fig. 11. (a) Phase error (ΔS) of the retrieved spectra compared to the ideal one for $\text{SiO}_2/\text{C}_{60}$ system, calculated from interferograms with different ZPD positions. (b) Light source spectrum used to calculate the interferograms in Fig. 10. (c) phase and (d) amplitude spectra calculated from the corresponding interferograms. The dramatic effect of changing interferogram asymmetry is obvious in both amplitude and phase spectra.

348 We recalculated the interferograms for the same sample as before with a Gaussian spectrum
 349 centered at 1300 cm^{-1} with an $\text{FWHM} = 200\text{ cm}^{-1}$. The corresponding interferograms are shown
 350 in Fig. 10. The figure shows that the spatially spread interferograms get distorted at smaller ZPD
 351 shifts than that of the broadband spectrum interferograms. Likewise, the spectral error of each
 352 shifted position, shown in Fig. 11 (a) reveals that a strong deviation of the resulting spectrum
 353 from the ideal occurs when the ZPD position is not chosen correctly.

354 We studied the effect of the interferogram width on the ideal position of the interferogram

and calculated the ideal ZPD position based on the minimum of the phase error for several light source spectra with different spectral widths. For all calculations, the phase error (ΔS) was calculated for the same spectral region between $\nu_1 = 900 \text{ cm}^{-1}$ and $\nu_2 = 1700 \text{ cm}^{-1}$. The results presented in Fig. 12 clearly show that with decreasing spectral width, the optimum ZPD position is further and further away from the beginning of the scanner range.

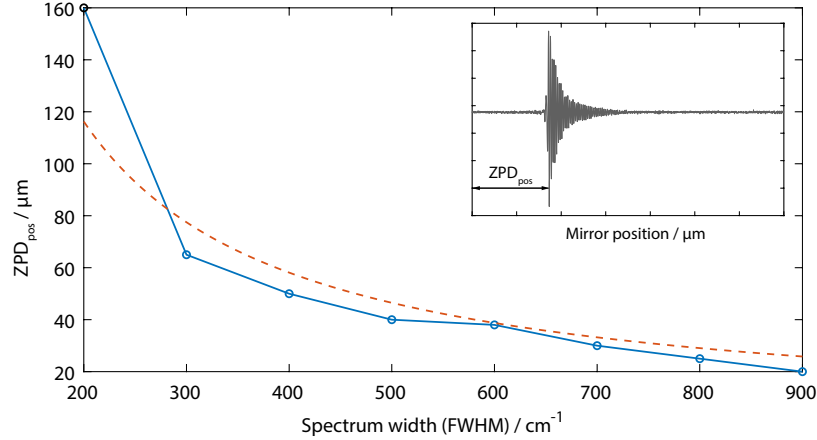


Fig. 12. Ideal ZPD position for different input spectrum widths (blue circles). The red dashed curve shows Eq. 12. The ZPD position is measured from the beginning of the scanner range as depicted in the inset.

We also aim to formulate how to find the ideal ZPD position depending on the spectral width of the light source. For the sake of simplicity, let us consider a light source with a Gaussian spectrum. From the FWHM of the light source spectrum (Δ_{LS}), we can calculate the width of the envelope of the interferogram (Δ_{IFG}), because the Fourier transform of a Gaussian is going to be also a Gaussian, thus:

$$\Delta_{IFG} = \frac{2}{\pi} \ln 2 / \Delta_{LS} \approx 0.44 / \Delta_{LS}. \quad (11)$$

As discussed, we want to keep the original shape of the interferogram as much as possible, thus the ZPD position has to be chosen accordingly. The ZPD position explicitly determines the steepness of the apodization function on both sides. To preserve the interferogram's shape we define a requirement that the 95% value point of the Blackmann-Harris apodization function has to coincide with the 50% point of the interferogram envelope (depicted in Fig. S5). This requirement results in

$$ZPD_{pos} \approx 2.3 / \Delta_{LS}. \quad (12)$$

In Eq. 12, ZPD_{pos} is measured from the beginning of the scanning range to easily implement during the scanner alignment. The result is plotted in Fig. 12 as the red dashed curve. Implementing this metric ensures that the spectrum is close to ideal and spectral phase component artifacts are minimized. Despite the good agreement between the derived formula and the numerical results, we want to note that it was derived for perfectly Gaussian light spectra resulting in a Gaussian interferogram envelope. In a more complex light spectrum, the interferogram can extend further to negative ZPDs thus being more vulnerable to the apodization. However, Eq. 12 can give a good approximation for the ZPD positioning, and the interferogram formulas in Eq. 8 help for more detailed analyses if needed. More details on the derivation of the optimal ZPD position equation can be found in the Supplementary Information material.

5. Conclusion

We showed that experimental nano-FTIR interferograms can be reproduced and understood in the framework of dispersive Fourier transform spectroscopy by choosing the proper insertion loss function defined by s-SNOM scattering models. Through simulations, we explained the ambiguity of coherent and non-coherent interferogram formation. We assessed the effect of apodization on the final spectrum and found that the preservation of interferogram asymmetry is key to obtaining an artifact-free phase spectrum. Based on our simulations, we provided a formula, for the first time, to determine an ideal shift for the ZPD position relative to the scanning range of the interferometer as a function of light source parameters.

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8. Disclosure

The authors declare no conflicts of interest.

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