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ON THE EFFICIENT FREQUENCY ESTIMATION OF A SINGLE TONE

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ABSTRACT

The frequency estimation of a single tone corrupted by additive white Gaussian noise has received significant attention over the last decades due to its wide applicability in signal processing. In this paper, we propose a computationally fast and statistically improved hybrid single tone estimator which outperforms other recently proposed approaches, lowering the signal-to-noise ratio at which the Cramér-Rao lower bound is closely followed. Numerical simulations indicate that, in contrast to many other techniques, the performance of the hybrid estimator is essentially independent of the underlying frequency component.

1. INTRODUCTION

In a wide variety of application areas, such as biomedicine, communications and radar, one often encounters a need to find a low computational complexity estimate of the dominant frequency component of data which are assumed to consist of a single complex sinusoid corrupted by additive white Gaussian noise, and the topic has, as a result, attracted significant interest over the last decades (see, e.g., [1–14], and the references therein). The problem can be briefly stated as follows; consider the data sequence

$$y(t) = \beta e^{i(\omega t + \theta)} + n(t), \quad (1)$$

where $\beta \in \mathbb{R}$, ω and $\theta \in [0, 2\pi)$ denote the deterministic but unknown amplitude, frequency, and initial phase, respectively, of a complex sinusoid. Further, $n(t)$ is a circular zero mean complex white Gaussian noise with variance σ_n^2 . Then, given the sequence $y(t)$, for $t = 0, \dots, N - 1$, the problem is simply to estimate ω with a low computational complexity and statistically efficient estimator. In [2], Rife and Boorstyn derived the maximum likelihood (ML) estimator of ω and proposed a statistically efficient approximate ML approach involving both a combined coarse and fine search, requiring $\mathcal{O}(N \log N)$ operations. Since then, a variety of phase-based methods requiring only $\mathcal{O}(N)$ operations have been developed. In [3], for example, Tretter

proposed a phase-based approach simplifying the problem to a linear regression on the phase. The method is based on a phase unwrapping algorithm, requiring a very high signal-to-noise ratio (SNR) ($SNR \gg 1$), here defined as $SNR = \beta^2 / \sigma_n^2$, to work well. Later, Kay proposed a modified version of Tretter's algorithm avoiding the use of the phase unwrapping algorithm [4]. The method, here termed Kay's weighted phase average (KWPA) estimator, can be shown to attain the Cramér-Rao lower bound (CRLB) for sufficiently high SNR, but the method is in general biased, and the SNR for which the CRLB is achieved depends on the underlying frequency [6, 8, 12]. As a result, the focus of recent contributions has mainly been aimed at reducing the SNR threshold [10], the frequency dependency of the threshold [7], or both [11, 14].

In this paper, we propose a computationally fast and statistically improved method, termed the hybrid estimator, combining the ideas in [10, 11, 14] to improve the performance further. The hybrid estimate is based on an initial coarse estimate of the unknown frequency using the uniformly weighted linear predictor (UWLP) method [1, 4]; this estimate is used to remove the frequency dependence of the SNR threshold. This SNR threshold is then further reduced via a combination of using an averaging filter, as suggested in [10], and an outlier removal scheme as proposed in [14]. Finally, a refined frequency estimate is formed along the lines proposed in [10, 11]. The resulting hybrid estimator only requires $\mathcal{O}(N)$ operations.

2. THE HYBRID PHASE-BASED FREQUENCY ESTIMATOR

As suggested in [3], the data model in (1) can be written as

$$y(t) = [1 + v(t)]\beta e^{i(\omega t + \theta)}, \quad (2)$$

where $v(t) = \beta^{-1}n(t)e^{-i(\omega t + \theta)}$ is a complex white sequence. Let $v_r(t)$ and $v_i(t)$ denote the real and the imaginary parts of $v(t)$, respectively. Then, for high SNR,

$$1 + v(t) \approx e^{i \arctan v_i(t)} \approx e^{i v_i(t)}, \quad (3)$$

allowing the approximation

$$y(t) \approx \beta e^{i\phi(t)}, \quad (4)$$

where $\phi(t) = \omega t + \theta + v_i(t)$. Most of the recent phase-based approaches exploit this approximation, allowing the phase to be approximately estimated from the difference of the adjacent phase values, i.e.,

$$\Delta\phi(t) \triangleq \arg[y^*(t)y(t+1)] \approx \omega + v_i(t+1) - v_i(t), \quad (5)$$

where $(\cdot)^*$ denotes the complex conjugate, suggesting the UWLP frequency estimator [1]

$$\hat{\omega}_c = \arg \left[\frac{1}{N-1} \sum_{t=0}^{N-2} y^*(t)y(t+1) \right]. \quad (6)$$

The UWLP estimator is unbiased, but statistically inefficient with variance [4, 8]

$$\text{var}(\hat{\omega}_c) = \frac{1}{(N-1)^2 \text{SNR}}. \quad (7)$$

As suggested in [7, 14], we will here use the UWLP estimate to form a downshifted signal, $y_d(t)$, to remove the frequency dependence of the SNR threshold, i.e.,

$$y_d(t) = y(t)e^{-i\hat{\omega}_c t}. \quad (8)$$

In [10], Kim *et al.* proposed using a simple K -tap averaging filter prior to the frequency estimation as a way to reduce the SNR threshold. Such an averaging can be shown to lower the SNR threshold up to $10 \log_{10} K$ dB. However, as such an averaging will severely restrict the allowed frequency range, the method in [10] is limited to signals with frequencies near zero. Herein, we note that the frequency content of the downshifted signal, $y_d(t)$, will satisfy such a restriction, and therefore propose to instead form an averaged signal as

$$y_f(t) = \frac{1}{K} \sum_{k=0}^{K-1} y_d(t+k). \quad (9)$$

Similar to (5), the adjacent phase difference of (9) can be formed as

$$\Delta\phi_f(t) = \arg[y_f^*(t)y_f(t+1)] = \omega_f + u_c(t), \quad (10)$$

where $u_c(t)$ is given by (23) for a general K . It is worth noting that the noise process $u_c(t)$ will now be *coloured* due to the average filtering [13].

As shown in [5], the SNR threshold behavior of the phase-based frequency estimators is affected by cumulative $\pm 2\pi$ phase errors resulting from the effect of the additive noise. This effect can be countered for by introducing an outlier detection scheme. Recently, an effective scheme

Figure 1: The MSE of the examined estimators as a function of the SNR.

was proposed in [14], where $\pm 2\pi$ outliers are detected if $|\beta_t| > |\beta_{t-1}|$, $|\beta_t| > |\beta_{t+1}|$ and $|\beta_t| > \lambda$, with

$$\beta_t = \Delta\phi_f(t-1) + \Delta\phi_f(t) + \Delta\phi_f(t+1), \quad (11)$$

where $\beta_{-1} = \beta_{N-K} = 0$ and $\Delta\phi_f(-1) = \Delta\phi_f(N-K) = 0$. Thus, the outliers can be removed as follows

$$\Delta\tilde{\phi}_f(t) = \begin{cases} \Delta\phi_f(t) - \text{sign}(\beta_t) 2\pi & \text{if outlier detected} \\ \Delta\phi_f(t) & \text{otherwise} \end{cases} \quad (12)$$

for $t = 0, \dots, N-K-1$. Here, λ is a user parameter; in the simulations below, we use $\lambda = 4$ (see [15] for a further discussion on the choice of λ).

After the SNR threshold reduction using (10) and (12), further improvement can be achieved by taking into account the colouration of the noise term in (10). This can be achieved using the FCFB approach suggested in [11]¹, whereby the frequency correction term, $\hat{\omega}_f$, can be found as

$$\hat{\omega}_f = \sum_{t=1}^{(N-K)/K} q(t) \sum_{m=1}^{K-1} \Delta\tilde{\phi}_f(tK-m), \quad (13)$$

where

$$q(t) = \frac{6tK(N-tK)}{N^3 - NK^2}, \quad (14)$$

with $t = 1, 2, \dots, (N-K)/K$. Combined with the coarse estimate, the hybrid frequency estimate is found as

$$\hat{\omega}_h = \hat{\omega}_c + \hat{\omega}_f. \quad (15)$$

¹It is worth noting that the FCFB applies a different set of weights than those used in the KWPA approach.

Figure 2: The MSE of the examined estimators as a function of the underlying frequency, for SNR = 6 dB.

In summary, the proposed hybrid estimator is found by first forming the downshifted signal in (8) using the UWLP estimate in (6). Then, the phase difference of the filtered signal is formed using (10), followed by the outlier removal scheme in (12). Finally, the refined frequency estimate is formed as (15), using (13). It is worth stressing that the hybrid method differs from previously suggested approaches in that it combines all the above steps; the FCFB method does not include the outlier removal scheme in (12). Similarly, the method proposed in [14], hereafter termed the outlier removal estimator (ORE), does not include the filtering in (10).

3. SIMULATIONS

In this section, we will briefly examine the performance of the proposed estimator. Initially, we consider $N = 24$ data samples containing a single complex sinusoid with frequency $\omega = 0.75\pi$, and examine the estimated mean square error (MSE) as a function of the SNR. Figure 1 illustrates the MSE for the proposed hybrid estimator, using $K = 6$, as compared to the UWLP approach [1], the FCFB approach following [11], the ORE approach [14], and the corresponding CRLB as given in [2]. As is clear from the figure, the performance of the proposed hybrid estimator is statistically improved, closely following the CRLB at a lower SNR threshold than the other examined methods. Further, the hybrid method uniformly yields a lower MSE than the other methods. It is worth noting that the hybrid estimator will suffer some performance degradation due to the introduced averaging in (9), as pointed out in [10]. This explains why the MSE of the proposed hybrid estimator can not exactly reach the CRLB as shown in Figure 1 and other figures. As

Figure 3: The MSE of the examined estimators as a function of the underlying frequency, for SNR = 4 dB.

is well known, the performance of single frequency estimators is often affected by the underlying frequency. Figures 2 and 3 illustrate how the MSE varies as a function of the frequency of the sinusoid, ω , for $SNR = 6$ dB and $SNR = 4$ dB, respectively. As seen in the figures, the hybrid estimator is uniformly achieving a lower MSE than the other approaches, and is essentially independent of the underlying frequency. It is clear from the figures that the FCFB approach is significantly affected by the underlying frequency, whereas the ORE approach is showing a similar robustness as the hybrid approach, although with a somewhat worse performance. All the simulation results in the paper have been obtained using 10^4 Monte-Carlo simulations. Finally, we remark that further simulations can be found in [15].

4. APPENDIX

In this appendix, we derive an expression for the noise process $u_c(t)$, given in (10), for a general K . Let $\omega_f = \omega - \hat{\omega}_c$. Then, using (2), $y_f(t)$ can be expressed as

$$y_f(t) = \frac{\beta}{K} e^{i\omega_f t + i\theta} \sum_{k=0}^{K-1} [1 + v(t+k)] e^{i\omega_f k}, \quad (16)$$

for $t = 0, \dots, N - K$. Introduce

$$\Psi_K \triangleq \sum_{k=0}^{K-1} e^{i(kK-1)\omega_f/K} \quad (17)$$

$$\Phi_v^K(t) \triangleq \sum_{k=0}^{K-1} v(t+k) e^{i(kK-1)\omega_f/K}. \quad (18)$$

Then,

$$\begin{aligned} y_f(t) &= \frac{\beta}{K} e^{i\omega_f t + i\theta + i\omega_f/K} [\Psi_K + \Phi_v^K(t)] \\ &= \frac{\beta\Psi_K}{K} e^{i\omega_f t + i\theta + i\omega_f/K} [1 + \Psi_K^{-1}\Phi_v^K(t)] \end{aligned}$$

Thus, the argument of $y_f(t)$ can be expressed as

$$\begin{aligned} \arg[y_f(t)] &= \arg[\Psi_K] + \omega_f t + \theta + \omega_f/K \\ &\quad + \arg[1 + \Psi_K^{-1}\Phi_v^K(t)], \end{aligned}$$

implying that the phase difference from adjacent samples, $\Delta\phi_f(t)$, can be expressed as

$$\Delta\phi_f(t) = \omega_f + u_c(t), \quad (19)$$

where, for $t = 0, \dots, N - K - 1$,

$$\begin{aligned} u_c(t) &\triangleq \arg[1 + \Psi_K^{-1}\Phi_v^K(t+1)] \\ &\quad - \arg[1 + \Psi_K^{-1}\Phi_v^K(t)] \end{aligned} \quad (20)$$

Then, using the approximation in (3), (20) can for high SNR be approximated as

$$u_c(t) \approx \text{Im} \{ \Psi_K^{-1} [\Phi_v^K(t+1) - \Phi_v^K(t)] \}, \quad (21)$$

where $\text{Im}\{x\}$ denotes the imaginary part of x . We note that, using a first-order Taylor expansion,

$$\Phi_v^K(t) \approx \sum_{k=0}^{K-1} v(t+k), \quad (22)$$

as ω_f is small due to the downshifting, implying that

$$u_c(t) \approx \text{Im} \{ \Psi_K^{-1} [v(t+K) - v(t)] \}. \quad (23)$$

We note that for $K = 2$, (23) yields the expression given in [10], i.e.,

$$u_c(t) \approx \frac{v_i(t+2) - v_i(t)}{2 \cos(\omega_f/2)}. \quad (24)$$

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